

Design and Analysis of Microstrip High Pass Filter Using Metamaterial

Rupam Shah¹, Dr. Awadhesh K.G. Kandu²

¹M.Tech Scholar, ²Associate Professor (EC), SORT, PU, Bhopal, India

Abstract--In this paper, design of six stubs i.e. six degree filter is being proposed and analyzed by using simulated S-parameters response with IE3D software. Also Highly selective filter based on complementary split ring resonator is pointed out. The structure shows a composite right or left handed (CRLH) behavior and, by properly tuning the geometry of the elements, a high pass response with a sharp transition band is achieved. Since the resonant elements are small, filter dimensions are compact .It comprises two CSRR sections with additional microstrip patches. The inter-digital capacitors are introduced to prevent transmission at lower frequencies. Left handed micro-strip lines are implemented by etching CSRRs in the ground plane and series capacitive gaps in the signal strip.

Index Terms- composite right/left handed (CRLH), CSRR, and IE3D.

I. INTRODUCTION

Micro-strip filters are the two port network used to control the frequency response at a certain point in a microwave system by providing transmission at frequencies within the pass band of the filter and attenuation in the stop band of the filter. RF/microwave filters may be designed as lumped element or distributed element circuits. Micro-strip filters are of four types namely; low pass filter, high pass filter, band reject filter and band pass filter.

The term "metamaterial" refers to any material that is artificially constructed with the purpose of achieving desired properties. In electro-magnetics, a meta-material can be created from a structure with elements of size less than the wavelength of the incoming electromagnetic wave. One important type of meta-material is the left-handed meta-material.

J. B. Pendry proposed a structure, which is named as split ring to produced negative effective permeability in microwave (GHz) range.

The synthesized capacitance, together with the natural inductance of split ring cylindrical structure, makes split rings resonant and has an effective relative permeability as follows:

$$\mu_{eff} = 1 - \frac{\pi r^2 / a^2}{1 - \frac{2\sigma i}{\omega r \mu_0} - \frac{3dc_0^2}{\pi^2 \omega^2 r^3}} \quad 1.1$$

Where r is the radius of split ring, a is the spacing distance between rings, and d is distance between inner and outer rings. It is apparent that the split ring resonator (SRR) will achieve resonance and large effective permeability at resonance frequency $\omega_0 = \sqrt{\frac{3dc_0^2}{\pi r^3}}$. Also the effective permeability will show negative values when second term of above equation is greater than unity, which corresponds to the frequency range between resonance frequency and magnetic plasma frequency

$$\omega = \omega_0 \sqrt{1 - \frac{\pi a^2}{r^2}} \quad 1.2$$

Split Ring Resonators (SRR) and Complementary Split Ring Resonators (CSRRs) are widely used to design meta-material structures. These structures when excited by suitable electromagnetic fields have resonance behaviour and show unusual properties such as negative permeability and permittivity near the resonance frequency region. Also, because of their resonance behaviour SRRs and CSRRs can be used to design slow wave transmission lines, phase shifters, various kinds of micro-strip filters, etc. SRRs are small resonant particles with a high quality factor at microwave frequencies. The SRR can be viewed as an externally driven LC circuit with a resonant frequency tunable by device dimensions (r , c , and d). The resonant frequency is

$$\omega_0 = \frac{1}{\sqrt{LC}} \quad 1.3$$

or

$$f_0 = \frac{1}{2\pi} \sqrt{\frac{2}{\pi r_0 L C_{pull}}} \quad 1.4$$

Where C_{pull} is the per unit length capacitance between the concentric rings, L is the total inductance of the SRR, and r_0 is the average radius of the SRR. To excite optimally the SRR, the incident H-field needs to be polarized in the axial direction of the ring. This can be done in micro-strip technology placing the rings in the same plane as the conductor strip. But this solution makes difficult the integration of the rings in the same area than other parts of the circuit. This problem is solved by using the complementary SRR (CSRR).

II. STUB MICROSTRIP HIGH PASS FILTER USING VIA HOLE GROUNDING

Fig 1.1 shows the proposed six stubs (short-circuited) optimum distributed high pass filter. The design parameters under consideration are as follows:

Cut-off frequency, $f_c = 1.5$ GHz

Dielectric Constant, $\epsilon_r = 4.4$

Height of substrate, $h = 1.6$ mm

Pass band ripple = 0.1dB

Characteristic impedance of terminating micro-strip line, $Z_0 = 50\Omega$

Effective permittivity of the micro-strip, $\epsilon_{eff} = 3.0622$

Guided wavelength, $\lambda_{gc} = 65.77636$ mm

Number of stub elements, $n = 6$

Electrical length, $\theta_c = 33$ degree (0.588 radians)

III. PROPOSED GEOMETRY OF SIX STUBS FILTER

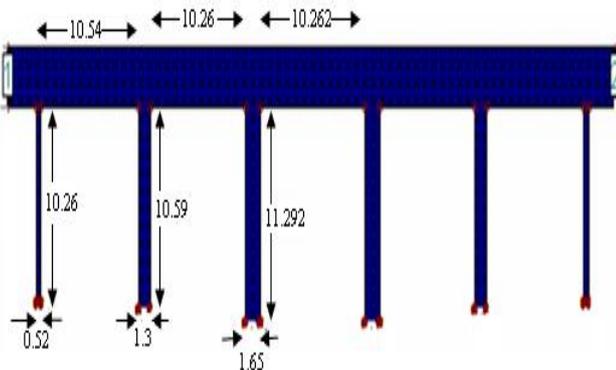


Fig 1.1: Proposed Geometry of Six Stubs Filter ($f_c = 1.5$ GHz)

IV. COMPARATIVE ANALYSIS OF SIMULATED AND MEASURED RESULTS

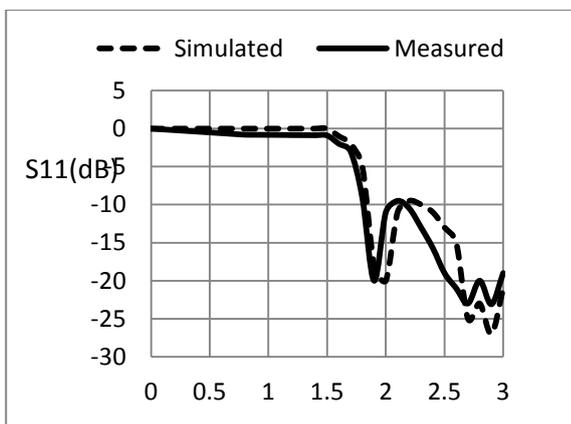


Fig. 1.2 Return Loss versus Frequency

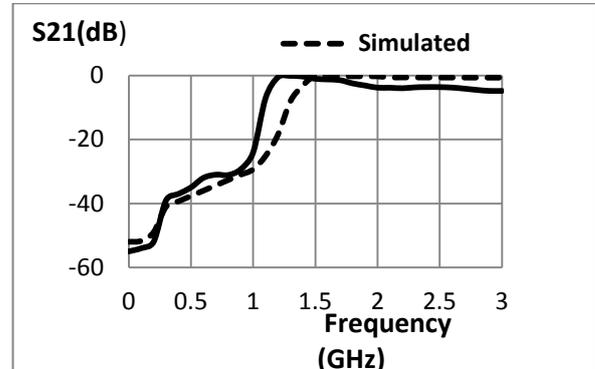


Fig 1.3 Transmission Coefficient versus Frequency

V. DESIGN OF HIGH PASS FILTER USING CSSRS

The substrate characteristics are:

Dielectric Constant $\epsilon_r = 4.4$

Thickness $H = 1.6$ mm

Tangent Tan $\Delta = 0.02$

Filter Dimensions Are:

Radius of the CSRRS , $r_{ext} = 16.91$ mm

Width of the Inner Ring = 1.99 mm

Width of the Outer Ring = 1.49mm

Rings Separation $D = 1.45$ mm

Number of Fingers = 14

Width of each Finger = 1.08 mm

Separation between each Finger = 1.08 mm

Line width $W = 1.35$ mm

Total filter length = 108 mm

VI. SIMULATED GEOMETRIES

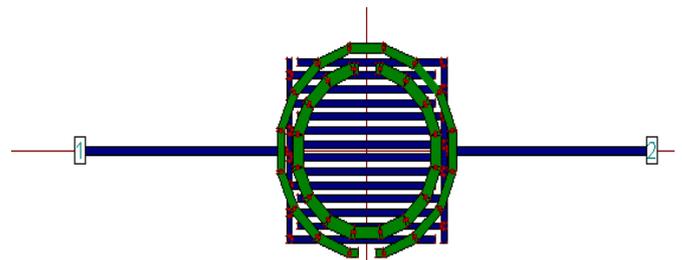


Fig. 1.4 Simulated Geometry of Single Stage CSRR Based High Pass Filter

VII. COMPARATIVE ANALYSIS OF SIMULATED AND MEASURED RESULTS

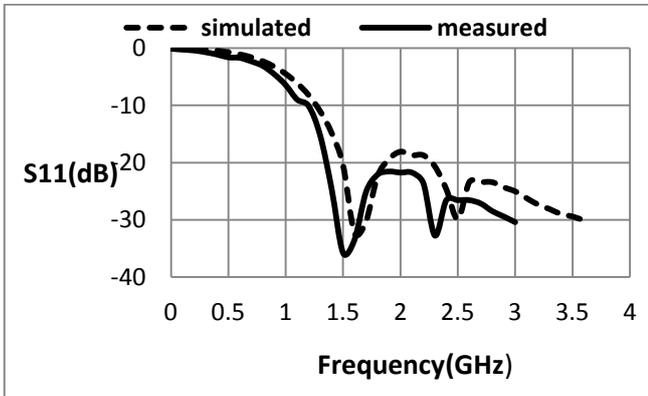


Fig.1.5 Return Loss versus Frequency

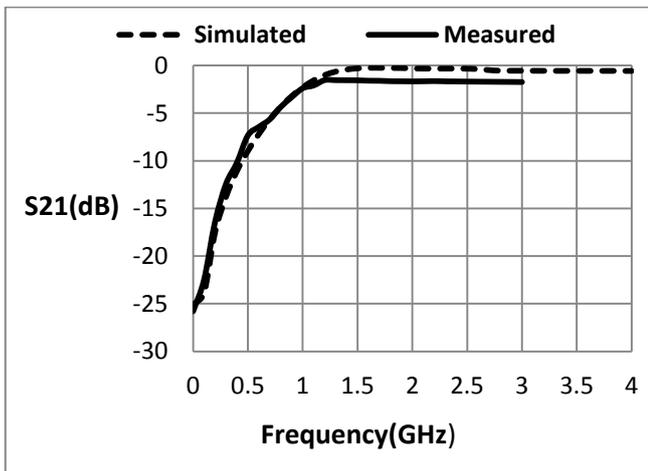


Fig. 1.6 Transmission Coefficient versus Frequency

VIII. HIGH PASS FILTER BASED ON CSRRs HAVING TWO STAGES

Fig.1.7 shows the layout of the proposed high pass filter having two stages of inter-digital high pass section. It comprises two CSRR sections with additional micro-strip patches. The inter-digital capacitors are introduced to prevent transmission at lower frequencies. The length of the transmission line embedded between the two sections can be adjusted to optimize the response of the total structure, which is similar to the elliptic function circuit [11]. The dimensions are:

$l = 8\text{mm}$, $w_1 = 1.4\text{mm}$, $s_1 = 2\text{mm}$
 $s_2 = 2\text{mm}$, $g_1 = 0.4\text{mm}$, $g_2 = 2.4\text{mm}$, $l_1 = 21.6\text{mm}$
 Total length = 104 mm.

The measured 3 dB cut off frequency is 2.6 GHz and the suppression is more than 19 dB below 2.2 GHz.

It can be seen that the proposed high pass filter exhibits steep rejection slope owing to the resonance of the CSRRs. Split Ring Resonators (SRR) and Complementary Split Ring Resonators (CSRR) are widely used to design meta-material structures. These structures when excited by suitable electromagnetic fields have resonance behaviour and show unusual properties such as negative permeability and permittivity near the resonance frequency region [5].

IX. PROPOSED GEOMETRY

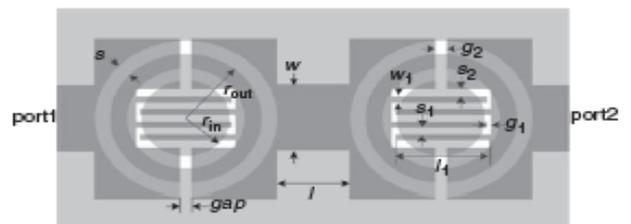


Fig. 1.7 Proposed Geometry of High Pass Filter

X. SIMULATED GEOMETRY

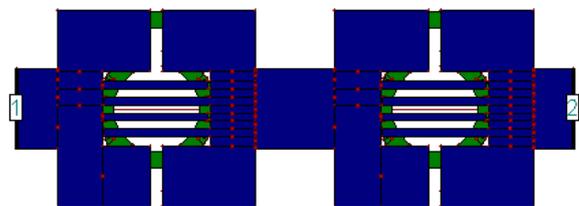


Fig.1.8 Simulated Geometry of CSRR

XI. COMPARATIVE ANALYSIS OF SIMULATED AND MEASURED RESULTS

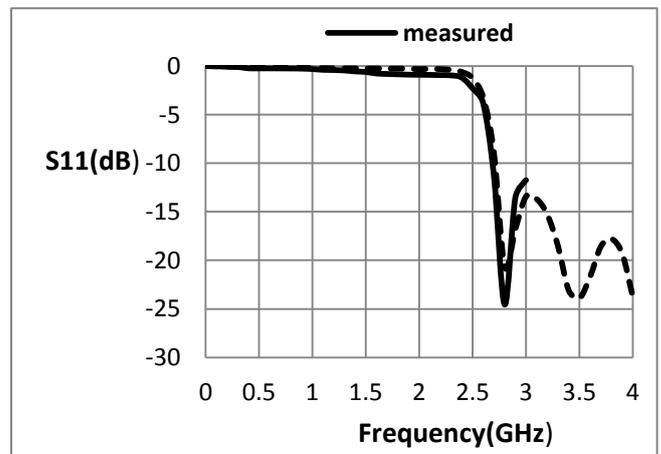


Fig.1.9 Return Loss versus Frequency

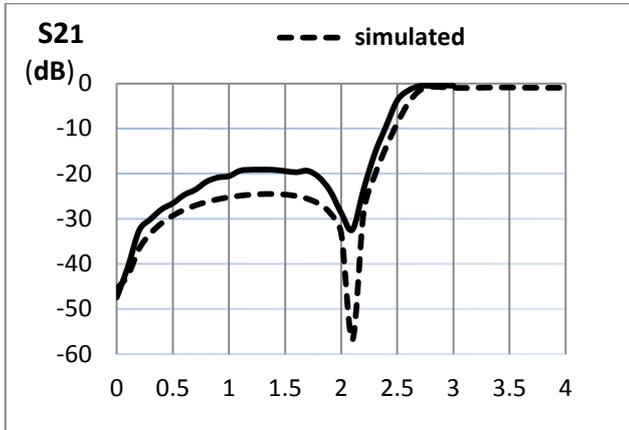


Fig.1.10 Transmission Coefficient versus Frequency

XII. CONCLUSION

In this paper, three compact micro-strip high pass filters using via hole grounding, unit cell complementary split ring resonator, two cell complementary split ring resonator are implemented and examined.

REFERENCES

- [1] V.G. Veselago, "The electrodynamics of substances with simultaneously negative values of ϵ and μ ", Soviet Physics Uspekhi, Vol. 10, pp. 509-514, January-February 1968.
- [2] Xiao Wang, "Simulation of simultaneously negative medium meta-materials", Virginia Polytechnic Institute and State University, Virginia, pp. 13-17, 2009.
- [3] Jia-Shen, G. Hong & M.J. Lancaster, "Microstrip filters for RF/microwave applications," John Wiley & Sons Inc., 2001.
- [4] M.Gil, J. Bonache, J. Selga, J. Garcia-Garcia, and F. Martin, "High-pass filters implemented by composite right/left handed (crlh) transmission lines based on complementary split rings resonators (csrrs)", PIERS online, vol. 3, no. 3, 2007.
- [5] C. Li, K.-Y. Liu and F. Li, "Design of microstrip high pass filters with complementary split ring resonators" Electron. Lett., 43, pp. 35-36, 2007.
- [6] J.-C. Liu, D.-S. Shu, B.-H. Zeng, D.-C. Chang, "Improved equivalent circuits for complementary split-ring resonator-based high-pass filter with C-shaped couplings", IET Microw. Antennas Propag., vol. 2, no. 6, pp. 622-626, 2008.
- [7] F. Aznar, M. Gil, J. Bonache and F. Martín, "Revising the equivalent circuit models of resonant-type metamaterial transmission lines", IEEE MTT-S International Microwave Symposium Dig., pp. 323-326, Atlanta (USA), June 2008.
- [8] Marta Gil, Jordi Bonache, Joan García-García, Jesús Martel, and Ferran Martín, "Composite right/left-handed metamaterial transmission lines based on complementary split-rings resonators and their applications to very wideband and compact filter design", IEEE transactions on microwave theory and techniques, vol. 55, no.6, June 2007.
- [9] Caloz C., Itoh T., "Electromagnetic metamaterials: transmission line theory and microwave applications", John Wiley & Sons, New Jersey, 2005.
- [10] Baena J.D., Bonache J., Martin F., Sillero R.M., Falcone F., Lopetegui T., et al, "Equivalent-circuit models for split-ring resonators and complementary split-ring resonators coupled to planar transmission lines", IEEE trans. microw. theory tech., 53, pp. 1451-1461, 2005.
- [11] Bonache J., Gil M., Gil I., Garcia J., Martin F., "On the electrical characteristics of complementary metamaterial resonators", IEEE Microw. Wirel. Compon. Lett., 16, pp. 543-545, 2006.
- [12] Pozar D.M., "Microwave engineering", Wiley, New York, 3rd edition, 2005.
- [13] IE3D, version 10.2, Zeland Corp, Fremont, CA.